

INCONEL® alloy 725 (UNS N07725) is a nickelchromium-molybdenum-niobium alloy that is highly resistant to corrosion and is age hardenable for extremely high strength. It has essentially the same corrosion resistance as INCONEL alloy 625, which is widely used in a broad range of severely corrosive environments. The strength of age-hardened INCONEL alloy 725 is of the order of twice that of annealed alloy 625. Because the strength of alloy 725 is developed by heat treatment, not by cold work, ductility and toughness remain high. Also, strength can be imparted to large or non-uniform sections that cannot be strengthened by cold work.

The chemical composition of INCONEL alloy 725 is given in Table 1. High levels of nickel and chromium provide corrosion resistance in reducing and oxidizing environments. The substantial molybdenum content enhances resistance to reducing media and provides a high degree of resistance to pitting and crevice corrosion. Additionally, the combination of elements makes the alloy resistant to hydrogen embrittlement and stresscorrosion cracking.

The properties of INCONEL alloy 725 are useful for a range of applications that require outstanding corrosion resistance along with high strength. The alloy is used for hangers, landing nipples, side pocket mandrels and polished bore receptacles in sour gas service, where it resists the effects of hydrogen sulfide, chlorides and carbon dioxide. The alloy is also attractive for high strength fasteners in marine applications, where it resists corrosion, pitting and crevice attack in seawater.

Table 3 - Thermal and Electrical Properties

Temperature	Coefficient of Expansion	Electrical Resistivity
° 3° 3° 3° 3°	in/in-°F	ohm-cmil/ft
70	15" And 17" 15"	688.3
200	7.22	696.2
400	7.21	710.4
600 🧹 🍼	7.44	727.1
800	7.68	741.3
1000	7.79	758.6
1200	8.05	761.7
1400	8 8 5 5	້ 776.1
1600		784.6
°C	µm/m-°C	µohm-m
20		1.144
i 100	13.0	1.158
200	13.1	1.179
300	13.4	1.206
400	13.7	1.226
500	14.1	1.251
600	14.4	1.265
700	atterned atterned atterned atterned	1.273
800		1.302

^aMean coefficient of linear expansion between 70°F (21°C) and temperature shown.

Table 1 -	Chemical	Composition,	%
-----------	----------	--------------	---

Nickel	
Chromium	
Molybdenum	
Niobium	
Titanium	
Aluminum	0.35 max.
Carbon	
Manganese	0.35 max.
Silicon	0.20 max.
Phosphorus	0.015 max.
Sulfur	
Iron	Balance*

*Reference to the 'balance' of a composition does not guarantee this is exclusively of the element mentioned but that it predominates and others are present only in minimal quantities.

Physical Properties

Some representative physical properties of INCONEL alloy 725 are given in Table 2. Values for thermal expansion and electrical resistivity over a range of temperatures are listed in Table 3. Resistivity at elevated temperature was calculated from observed percent change in the room-temperature value. Modulus of elasticity, determined dynamically, is given in Table 4. All values for physical properties are for material in the age-hardened condition.

Table 2 - Physical Properties

Density, Ib/in ³	0.300
g/cm ³	8.31
Melting Range, °F	2320-2449
°C	1271-1343
Permeability at 200 oersted (15.9 kA/m)	<1.001
Young's Modulus (70°F), ksi x 10 ³	
GPa	204
Shear Modulus (70°F), ksi x 10 ³	
GPa	
Poisson's Ratio (70°F)	0.31



INCONEL® alloy 725

Temperature	Young's M odulus	Shear Modulus	Poisson's Ratio	Temperature	Young's M odulus	Shear Modulus	Poisson's Ratio
°F	ksi x 10 ³	ksi x 10³		°C ,	GPa	GPa	and a startman a startman and startman atter
70	29.6	11.3	0.31	20	204	78	0.3
200	29.1	11.1	0.31	100	200	76	0.3
400	28.2	10.7	0.32	200	J 194	74	0.3
600	27.2	10.3	0.32	300	.188	71 /	0.3
800	26.3	9.9	0.33	400	182	69	0.3
1000	25.4	9.6	0.32	500	177	67	0.3
1200	24.0	9.0	0.33	600	169	63	J J J J J 0.3
1400	22.5	8.4	0.34	700	160	61	0.3
1600	21.2	7.9	0.34	800	150	56	0.3

Table 4 - Dynamic Modulus of Elasticity

Table 3a - Thermal Conductivity and Specific Heat Values for INCONEL alloy 725

Temperature, °C	Temperature, °F	Thermal Co	nductivity	Specif	ic Heat
and Statement Statement Statement	Part Statement Statement Statement	W/m K	BTU in/ft ² h °F	J/kg °C	BTU/lb °F
23	73	10.631	73.76	430	0.103
93	200	11.724	81.34	446	0.107
100	212	11.827	82.06	447	0.107
s 149 s s	300	12.666	87.88	457	0.110
200	392	13.544	93.97	468	0.112
204	400	13.615	94.46	469	0.113
260	500	14.491	100.54	481	0.115
300 🗸 🗸	572	15,122	104.92	489	0.117
316	600	15.390	106.78	492	0.118
371	700	16.346	113.41	503	0.121
400	752	16.843	116.86	508	0.122
J 427 J J	800	17.284	119.92	511 5	0.123
482	900	17.920	124.33	517	0.124
500	932	18.152	125.94	519	0.125
538	1000	18.864	130.88	531	0.127
່ 593 ໍ່	1100	19.912	138.15	້ 550 ັ	0.132
600	1112	20.037	139.02	552	0.133
649	1200	21.205	147.12	577	0.139
700	1292	22.424	155.58	604	0.145
704 🗸 🗸	1300	22.453	155.78	ో 604 ో	0.145
760	1400	22.807	158.24	607	0.146
800	1472	23.062	160.01	609	0.146
816	1500	23.179	160.82	610	0.146
َ ^{لَ} 871 کَ	1600	23.596	163.71	615	0.148
900	1652	23.812	165.21	618	0.148
927	1700	24.226	168.08	624	0.150
982	1800	25.086	174.05	635	0.152
1000 🕤 🚽	1832	25.361	175.96	639	0.153
1038 🚽 🗧	1900	25.994	180.35	645	0.155
1093	2000	26.925	186.81	653	0.157
1100	2012	27.038	187.59	654	0.157
1149	2100	28.292	196.29	663	0.159
1200 🗸 🗸	2192	29.604	205.39	673 🖉 🦪	0.163

Mechanical Properties

In the age-hardened condition, INCONEL alloy 725 displays high strength along with excellent ductility and toughness. Mechanical properties over a range of temperatures are shown in Figures 1 and 2. Table 5 gives typical tensile properties, hardness, and impact strength for various product forms. The data in Table 6 indicate the good flattening properties of age-hardened tubing. Table 7 lists the average high-temperature tensile properties for annealed + aged bar, 0.625 to 6.5 inches (16 to 165 mm) diameter.

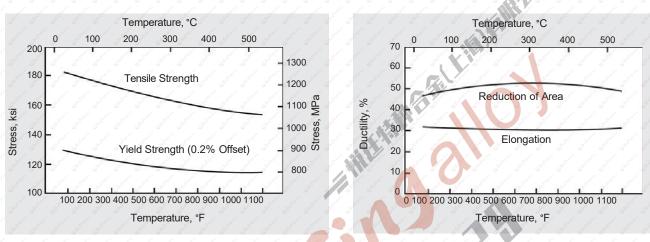


Figure 1. Tensile and yield strength of INCONEL alloy 725.

Figure 2. Elongation and reduction of area of INCONEL alloy 725.

Form	Condition	Yield St (0.2% (1100 LCC	isile ngth	Elongation	Hardness	Cha	rpy Impact
	Set Set Set Set Set Set	ksi	MPa	ksi	MPa	%	Rc	ft-lbf	Jan Jan Star
Rounda	Annealed	62.0	427	124.0	855	57	5	- 68	- 92
	Age Hardened	133.0	917	180.0	1241	ి 30 ో	ు 36 ో	in States States	
Round ^b	Age Hardened	131.0	903	180.0	1241	31	36	97	132
Tube	Annealed	48.4	334	113.6	783	60	5	and states and	" Straff" - Straff" Straff
	Age Hardened	133.6	921	183.9	1268	27	39	all and and	, Or Or Or

Table 5 - Typi	ical Room	Temperature	Mechanical	Properties
----------------	-----------	-------------	------------	------------

^aTransverse specimens from hot-finished rounds of 4.0 to 7.5 in (102 to 190 mm) diameter.

^bLongitudinal specimens from hot-finished rounds of 0.5 to 7.5 in (13 to 190 mm) diameter.

Note: The above mechanical properties are "mean" values, and do not represent variances resulting from differences in thermo-mechanical processing.

	Yield St (0.2%		Hardness	Flattening*
× .	k si 🗸	MPa 🚽	o R _c o o	3 ¹⁰ 3 ¹⁰ % 3 ¹⁰ 3 ¹⁰
	117	807	-36	>52.8
Provin	133	917	39	38.8

Table 6 - Flattening	Tests on Ag	ge-Hardened	Tubing	
----------------------	-------------	-------------	--------	--

*Reduction in diameter at 5% drop in load of ring specimen from tubing 2.375 in (60 mm) outside diameter and 0.217 in (5.5 mm) wall.

Tempe	erature	ture Yield Strength (0.2% Offset)		Tensile Strength		Elongation	Reduction of Area
°F	°C	ksi	MPa	ksi	MPa	%	%
75	23	129.4	892	181.9	1254	32.0	48.4
100	38	131.7	908	182.2	1256	32.6	49.2
200	93	125.9	868	178.4	1230	29.6	47.0
300	149	119.8	826	172.4	1189	30.9	50.2
400	204	119.5	824	169.7	1170	30.7	52.4
500	260	117.6	811	165.5	/ 1141	31.0	52.7
600	315	113.4	782	159.5	1099	32.4	54.2
650	343	117.4	809	159.8	1102	31.1	53.5
700	371	115.7	798	158.9	1096	30.8	53.4
750	399	115.9	799	157.8	1088	30.8	53.9
800	426	118.6	818	160.4	1106	29.6	49.6
850	454	114.6	790	155.3	1071	31.5	51.6
900	482	117.1	807	155.9	1075	30.7	49.7
950	510	111.6	769 🧉	154.4	1065	31.7	of 50.1
1000	538	112.9	778	153.4	1058	31.0	47.7

Table 7 - Average High-Temperature Properties for 0.625 to 6.5 in (16 to 165 mm) Diameter Rod, Annealed + Aged*

* Solution treated at 1900°F (1038°C) then aged at 1350°F (732°C)/8 h/FC at 100°F (56°C)/h to 1150°F (621°C)/8 h/AC.

Corrosion Resistance

High nickel, chromium and molybdenum contents enable INCONEL alloy 725 to resist a broad range of corrosive environments. The alloy is especially resistant to media containing carbon dioxide, chlorides and hydrogen sulfide, such as those encountered in deep sour gas wells. In such environments, INCONEL alloy 725 resists corrosion, pitting, hydrogen embrittlement and stress-corrosion cracking. Table 8 shows the performance of the alloy in a standard test (NACE TM0177) used to determine resistance to sulfide stress cracking (hydrogen embrittlement) in a sour well environment. Table 10 shows the alloy has good resistance to stress-corrosion cracking at temperatures up to about 450°F (230°C) in a severe sour environment containing elemental sulfur. INCONEL alloy 725 is approved under NACE MR0175 for use in sour gas wells.

INCONEL alloy 725 displays excellent resistance to general and localized corrosion in brines and sea water. Table 11 shows the results of crevice corrosion tests in sea water. These data show alloy 725 to be superior to alloy 625 in resistance to crevice corrosion initiation.

Figure 3 shows the results of C-ring laboratory tests, in a severely aggressive 25% NaCl, 0.5% acetic acid, 1g/l sulfur environment, with 120 psi (825 kPa) hydrogen sulfide. Figure 4 plots mean axial stress vs. cycles of fatigue for INCONEL alloy 725 in the dual aged condition [1350°F (732°C)/8h, FC@100°/h., 1150°F (621°C)/8h/AC].

Alloy	Material	Yield St (O.2%	trength Offset)	Hardness	Duration	Sulfide Stress
Alloy	Condition	ksi	MPa	R _c	Days	Cracking
INCONEL alloy 725	Cold Worked	90.0	621	25	30	No
least Steat Start Steat Start	Age Hardened	117.6	811	్ 37 ్	× 30 × ×	o No o
enter character character character of	Age Hardened	128.6	887	40	30	No 🖉
to the state of th	Age Hardened ^b	130.8	902	41.5	30	No
and and and and and	Age Hardened	132.9	916	36	42	No
ter ster ster ster s	Age Hardened	133.0	917	39	30	No
terrar Starrar Starrar Starrar Starrar	CW & Aged	137.8	950	39	42	No s
INCONEL alloy 625	Cold Worked	125.0	862	30.5	42	No
that the taken that the	Cold Worked	160.0	1103	37.5	10	Yes
and the state of the	Cold Worked	176.0	1214	41	6	Yes
INCONEL alloy 718	Age Hardened	120.0	827 3	30	42 3 3	S No S
harmon alla tan alla tan alla tan alla tan alla tan	Age Hardened	130.0	896	37	42	No
And And And And	Age Hardened	134.0	924	38.5	42	No
	Age Hardened	139.0	958	38	42	No
ear oran oran oran oran	Age Hardened	156.0	1076	a 41 a a	of of 60 of of	of No of
and Statement Statement Statement Statement	Cold Worked	197.0	1358	37.5	2	Yes
south south south south south	Cold Worked	197.0°	1358°	37.5	25	Yes

Table 8 - C-Ring Tests in NACE Solution (TM0177)^a

^aRoom-temperature tests at 100% of yield strength in 5% NaCl plus 0.5% acetic acid saturated with H₂S. All specimens were coupled to carbon steel. ^bAlso exposed to a simulated well age of 600°F (315°C)/1000 h.

°Test stress was 84% of yield strength: 165 ksi (1138 MPa).

Table 9 - C-Ring Test Data Environment: 25% NaCl + 300 psig H₂S + 700 psig CO₂ + 1g/L S° at 350°F for 90 Days; Triplicate Specimens Stress to 100% of the 0.2% Yield Strength.

Alloy 725				and and and and and				No Cracking							6 ⁷	2 1
	5	1	ð N	25	37		5	3	S	S	S	S.	34	3W	3	্র

Sand Sand Sand Sand Sand Sand	Material	Yield Strength (0.2% Offset)		Stress-Corrosion Cracking at:							
Alloy	Condition	k si	MPa	350°F (177°C)	375°F (191°C)	4 00°F (204°C)	4 25°F (218°C)	4 50°F (232°C)	4 75°F (246°C)	5 00°F (260°C)	
INCONEL alloy 725	Age Hardened	117.6	811	No	No	No	No	No	Yes ^b	No	
and and and and and	Age Hardened	128.6	887	No	No	No	No	Yes		1	
Start Start Start Start Start	Age Hardened	132.9	916	No	S No	No	No	No	No	No	
Statute Statute Statute Statute Statute	Age Hardened	133.0	917	No	🖉 🖉 No	No 🧹	No	No	Yes ^b	No	
INCONEL alloy 625	Cold Worked	144.0	993	No	Yes	Start water with	1-1-	Start - Start	Strand with a	all state all	
C. C. C. C. C. C. S.	Cold Worked	160.0	1103	No	Yes	and and a				an 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
INCONEL alloy 718	Age Hardened	130.3	898	Yes	Star Star S			Stating Stating S	o ^{re} o ^{re}	S ^{tel} _ S ^{tel}	

Table 10 - Stress-Corrosion Cracking Tests in a Simulated Sour Well Environment a

^aC-ring autoclave tests of 14-day duration at 100% of yield strength in 25% NaCl plus 0.5% acetic acid plus 1g/l sulfur plus 120 psi (827 kPa) H₂S.

^bOne of two specimens cracked.

°At 275°F (135°C).

Table 11 - Crevice Corrosion Tests in Sea Water^a

Alloy	Condition	Corrosion Initiation	Sites Attacked	Depth Attacked		
Shaling Shaling Shaling	Sterrar Sterrar Sterrar	Days	%	s'in s'	mm	
INCONEL alloy 725	Age Hardened	Jahnen Jahnen Jahnen	0	0	0	
INCONEL alloy 625	Annealed	2-5	25-75	0.010	0.26 ^b	

^a30-day tests in flowing sea water at 86°F (30°C) with crevices formed by acrylic plastic washers bolted to sheet specimens.

^bAverage of maximum depth per crevice. Range of maximum attack was 0.0008 to 0.026 in (0.02 to 0.66 mm).

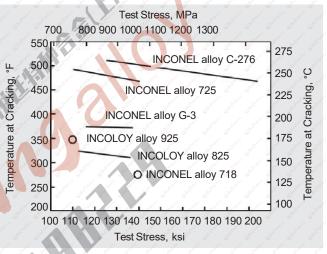


Figure 3 - Results of autoclave C-ring tests in a solution of distilled water containing 25% sodium chloride, 0.5% acetic acid, and 1 g/l sulfur with pressure of 120 psi (825 kPa) hydrogen sulfide. Test stresses were 100% of yield strength (0.2% offset).

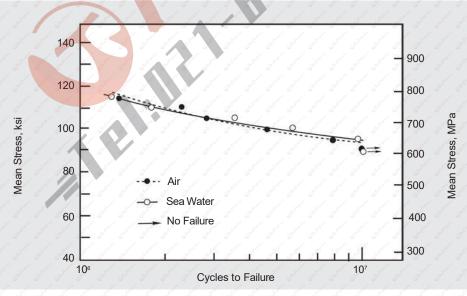


Figure 4 - Mean axial stress vs. cycles of fatigue for INCONEL alloy 725 in the dual aged condition [1350°F (732°C)/8h, FC@100°/h., 1150°F (621°C)/8h/AC] tension-tension test. Tested at the LaQue Center for Corrosion Technology. (R-value = Min. stress/Max. Stress=0.6)

Corrosion results for alloy 725 in mineral acids, compared to alloys 625 (N06625) and C-276 (N10276) are shown in Table 12. In all of the mineral acid environments of this study, both annealed and annealed plus aged alloy 725 exhibited corrosion resistance comparable to mill annealed alloys 625 and C-276.

Table 12 - Average Corrosion Rates for Alloy 725 (N07725) in Mineral Acids* Compared to Literature Data for Alloy 625 (N06625) and Alloy C-276 (N10276)

Alloy 725 Condition	1:	50°F 6°C)		HCI 0°F (66°C)	J	o HCI 50°F 6°FC)		iling H ₂ SO ₄	S S	iling HNO ₃		iling H ₃ PO ₄	Boil H₃PO₄	ing 80%
and the second second	mpy	mm/a	mpy	mm/a	mpy	mm/a	mpy	mm/a	mpy	mm/a	mpy	mm/a	mpy	mm/a
and 1 and the	<1	< 0.03	<1	< 0.03	105	2.67	25	0.64	<1	< 0.03	3	0.08	73	1.85
2	<1	<0.03	<1	<0.03	268	6.81	25	0.64	<1	< 0.03	5	0.13	62	1.57
3 3	∛ <1	<0.03	<1	< 0.03	250	6.35	25	0.64	<1	<0.03	3	0.08	45	1.14
J 4 J	<1	<0.03	<1	< 0.03	218	5.54	28	0.71	<1	< 0.03	2	0.05	35	0.89
Literature	alating and allating and	Andrew Andrew	aller alathon a	Internet atternet atternet	abetrain abe	Instruction of	better states	111.2.2	and sugar		J.S.	Jalan Jalan	Testinan Alestran	station station state
Alloy 625	<1	<0.03	69	1.75	93	2.36	18	0.45	<1	< 0.03	<10	<0.25	25	0.63
Alloy C-276	<5	<0.13	5-20	0.13-0.51	20	0.51	20	0.51	16	0.41	<5	<0.13	5-25	0.13-0.64

Two week duration

Condition: 1. 1900°F (1038°C) anneal

2. 1900°F (1038°C) anneal + 1400°F (760°C)/6h/AC

3. 1900°F (1038°C) anneal + 1375°F (746°C)/8h, FC at 100°F (56°C)/h to 1150°F (620°C)/8h/AC

4. 1900°F (1038°C) anneal + 1350°F (732°C)/8h, FC at 100°F (56°C)/h to 1150°F (620°C)/8h/AC

an an an an an an		Corrosion Rate								
Environment	Temperature	0- 96 H	lours	96-192 H	ours 🗸 🗸 🗸	0-192 Hours				
	°C (°F)	mpy	mm/a	mpy	mm/a	m py	m m/a			
0.2% HCI	Boiling	<0.1	<0.01	<0.1	<0.01	<0.1	< 0.01			
1% HCI	Boiling	4.6	0.12	1.9	0.05	10.2	0.26			
Staffor Staffar Staffor Staffar S	90 (194)	25.0	0.64	2.0	0.05	2.0	0.05			
5% HCI	70 (158)	193.8	4.92	203.3	5.16	169.7	4.31			
Statute Statute Statute	50 (122)	52.8	1.34	52.5	1.33	44.7	1.14			
	30 (86)	9.4	0.24	6.6	0.17	7.8	0.18			
10% H ₂ SO ₄	Boiling	9.9	0.25	21.5	0.55	4.6	0.12			
60% H ₂ SO ₄	70 (158)	25.5	0.65	25.6	0.65	16.0	0.41			
and the second second	50 (122)	23.1	0.59	0.71	0.02	29.0	0.74			
and a star and a star a	30 (86)	1.5	0.04	1.3	0.03	7.1	0.18			
95% H ₂ SO ₄	70 (158)	66.3	1.68	67.5	ి ి 1.71 ి	42.0	1.07			
and the second second second second	50 (122)	72.6	1.84	50.1	1.27	23.0	0.58			
The stand of the stand	30 (86)	11.0	0.28	13.3	0.34	13.0	0.33			
85% H ₂ PO ₄	Boiling	30.7	0.78	31.2	0.79	58.0	1.47			
State State State State	90 (194)	0.54	0.01	0.50	0.01	0.32	0.01			
80% CH ₃ CO ₂ H	Boiling	<0.1	<0.01	<0.1	< 0.01	<0.1	< 0.01			

Table 13 - Corrosion Rates for Alloy 725 (UNS N07725), 0.125-in. Sheet, Evaluated in Acid Environments for Varied Exposure Times and Temperatures as per MTI Manual No. 3 Procedures

Heat Treatment

INCONEL alloy 725 is strengthened by precipitation of gamma double-prime (γ ") phase during an aging heat treatment. Before it is aged, the material should be given a solution anneal at 1900°F (1040°C). Air cooling after solution annealing is the preferred cooling method.

For sour gas applications, the recommended aging treatment is 1350°F (730°C)/8h/furnace cool at 100°F (56°C)/h to 1150°F (620°C)/8h/air cool.

Welding

INCONEL alloy 725 welding products, designated INCO-WELD® Filler Metal 725NDUR®, provide a higher strength alternative to alloy 625 welding wire. Gas-tungsten-arc welding (GTAW) and gas-metal-arc welding (GMAW) are the preferred methods for welding INCONEL alloy 725. When GMAW is used, current levels should not exceed 180 amps for standard GMAW power sources in the "spray arc" metal transfer mode. Submerged-arc welding (SAW) and shielded-metal-arc welding (SMAW) are not recommended.

Table 14 shows average slow strain rate (SSR) ratio test data for 1-pass weld overlays in a 5% NaCl + 75 psig (517 kPa) $H_2S + 400$ psig (2758 kPa) CO₂ environment at 300°F (149°C). The most common pass/fail criterion for SSR testing is a ratio of time to failure (TTF), % reduction of area (% RA) and/or % elongation measured in a simulated oil patch environment relative to the same parameter in an inert environment (air). Ratios above 0.90 are considered acceptable "pass" levels.

The absence of secondary cracking indicates good stress-corrosion cracking resistance. INCONEL alloy 725, like alloy 625, show excellent resistance to stress-corrosion cracking.

Tables 15 and 16 respectively show room-temperature tensile and Charpy V-notch (CVN) impact test results for all-weldmetal samples of INCO-WELD Filler Metal 725NDUR in the as-welded, direct aged, and annealed-plus-aged conditions. Aswelded material exhibited excellent impact properties and lower yield strengths than the annealed-plus-aged material. The direct aged material exhibited low impact strength. Optimum results were obtained by annealing INCONEL alloy 725 prior to welding, then applying a solution anneal and age after welding.

Filler Metal	Time to Failure Ratio	% Reduction of Area Ratio	% Elongation Ratio	Secondary Cracking
INCO-WELD 725NDUR*	0.98	ar ar 1.11 ar ar a	1.00	No No
and shallow shallow shallow shallow shallow	1.07	0.97	1.11	And a second descent second descent descent descent
INCONEL alloy 625**	0.95	1.20	0.95	No No
Star Star Star Star Star and Star Star Star Star Star	0.90	0.92	0.90	en den den den den den den den generen generen generen generen generen generen

Table 14 - Slow Strain Rate Ratio Data

*Overlay on AISI 4140 steel, condition 1225°F (663°C) 2 h/AC.

**Overlay on AISI 4130 steel, condition 1175°F (635°C) 2 h/AC.

F = Fail

Test O rientation	Base Metal Pre-Weld	Post-Weld Treatment	Yield Strength		Tensile Strength		Elongation	Reduction of Area	Side Bend	
	Treatment	and a second and a second and a second	ksi	MPa	ksi	MPa	%	%	and and a second second	
Transverse	Annealed	As-Welded	73.6	507	124.9	861	39.0	34.4	P 2T	
Longitudinal	and transfer transfer to	As-Welded	76.0	524	119.8	826	33.0	30.6	P 2T	
Longitudinal	or or or or	Aged	130.1	897	172.1	1187	20.0	22.5	F 2T	
Transverse	Annealed	Aged	141.0	of 972	179.8	1240	13.0	19.5	🧳 P 4T 🗸	
Longitudinal	at a farmer a farmer a farmer a farmer	Annealed, Aged	129.9	896	173.9	1199	19.0	28.6	P 4T	
Transverse	Annealed, Aged	Annealed, Aged	131.8	909	171.4	1181	25.0	29.8	P 4T	
Longitudinal		Annealed(2), Aged	126.5	872	174.8	1205	21.0	28.4	P 4T	
Transverse	Annealed	Annealed(2), Aged	126.5	873	172.8	1191	28.0	42.7	🗸 P 4T 🗸	

Table 15 - Typical INCO-WELD Filler Metal 725NDUR All-Weld-Metal GMA Room-Temperature Tensile Properties

Age = 1350°F (732°C)/8 h/FC at100°F (56°C)/h to 1150°F (620°C)/8 h/AC

Table 16 - Typical INCO-WELD Filler Metal 725NDUR All-Weld-Metal GMA Impact Properties

Post-Weld Heat Treatment	CVN Impact at 75°F (24°C) CVN Impact at -75°F (-59°C						
	ft-lbf	J	ft-lbf	Jan Start Jack			
As-welded	66	89	and strange strange	Starter - Starter and			
1350°F (732°C)/8h/FC at 100°F (56°C)/h to 1150°F (620°C)/8h/AC	16	22	18	24			
1900°F (1038°C) anneal, plus		Stat Stat Stat Stat		the State State State			
1350°F (732°C/8h/FC at 100°F (56°C)/h to 1150°F (620°C)/8h/AC	42 🖉	57	39	53			
1950°F (1066°C) anneal, plus	and a strange astrony and	- tellester - tellester - tellester		and the state of t			
1350°F (732°C)/8h/FC at 100°F (56°C)/h to 1150°F (620°C)/8h/AC	56	76	79	107			

Hot Forming

Because of its strength, INCONEL alloy 725 is more resistant that most materials to deformation during hot forming. It is readily hot-worked if sufficiently powerful equipment is used.

Hot forming is performed in the 1650°-2050°F (899°-1121°C) temperature range. In the last operation, the metal should be worked uniformly with a gradually decreasing temperature, finishing with some light reduction in the 1650°-1750°F (899°-954°C) range. This procedure is necessary to ensure notch ductility in stress-rupture applications when material has been annealed and aged. In heating for hot working, the material should be brought up to temperature, allowed to soak a short time to ensure uniformity, and withdrawn.

To avoid duplex grain structure, INCONEL alloy 725 should be given uniform reductions. Final reductions of 20% minimum should be used for open-die work, and 10% minimum for closed-die work. Parts should be air-cooled from the hotworking temperature rather than water-quenched.

Care should be taken to avoid overheating the metal by heat buildup due to working. Also, the piece should be reheated when any portion has cooled below 1650°F (899°C). Preheating tools and dies to 500°F (260°C) is recommended. Any ruptures appearing on the surface of the workpiece must be removed at once.

Machining

INCONEL alloy 725 is an age hardenable alloy. Machining may be accomplished in the annealed or aged conditions. Excellent results have been obtained with SPC-633T tooling of KC-950 coated grade. For example, in a single-point turning of round stock, the cutting tool remained in good condition after turning 18 inches (457 mm) of bar length. The cutting speed was 55 surface feet (16.8 m)/min with 0.014 inches (0.36 mm) feed and 0.190 inches (4.8 mm) depth of cut. Other carbide tools and steel tools are listed in Table 17 with their recommended speeds, depths of cut, and feed rates.

Cemented carbide tools produce the highest cutting rates and are recommended for most turning operations involving uninterrupted cuts. High speed steel tools may be used for interrupted cuts, finishing to close tolerances, finishing with the smoothest surfaces, and cutting with the least amount of work hardening.

Chip Control

When machining INCONEL alloy 725, it is important to obtain good full turn chips. High speed steel tools may require chip curlers or lipped tools. The lip should be wider and deeper for the material in the annealed condition. Typical dimensions, for chip breakers, operating at 0.01 in/min (0.25 mm/min), are 0.020 inches (0.51 mm) deep and 0.080 inches (2.03 mm) wide.

Threading

Lathe Threading

Standard single-point lathe threading practices are adequate for threading INCONEL alloy 725 in the annealed or aged conditions. Recommended threading speeds are 3.0-3.5 ft/min (91-107 cm/min). The depth of cut will vary, becoming less as the work progresses.

Die Head Threading

Threading dies should be made of molybdenum high-speed steel (Grade M-2 or M-10). A chaser throat angle of 15 to 20° is recommended for producing V threads where no shoulder is involved. When close-to-shoulder threading must be done, a 15° rake angle is recommended. The speeds given for lathe threading also apply to die threading.

Thread Grinding

External threads can be produced in INCONEL alloy 725 by form grinding with aluminum oxide (150-320 grit) vitrifiedbonded grinding wheels. The recommended coolant is a high-grade grinding oil of about 300 seconds viscosity at 70°F (21°C). Extreme care must be taken to prevent overheating during grinding.

Drilling

Steady feed rates minimize excessive work hardening during drilling. Heavy duty, high speed drills with heavy webs are recommended. For twist drilling, recommended surface speeds are 10-12 ft/min (305-366 cm/min) for the annealed condition, and 8-10 ft/min (244-305 cm/min) for the aged condition. Feed rates range from 0.005 to 0.015 in/rev.(0.13 to 0.38 mm/rev.) depending on the drill size.

For gun drills, sizes from 1/16 to 2 inches (1.6 to 51 mm), a feed rate of 0.0001-0.003 in/rev. (0.003-0.08 mm/rev.) is recommended for both the annealed and aged conditions. The surface speed should be kept at about 100 ft/min (30.5 m/min) for annealed material and 60 ft/min (18.3 m/min) for material in the aged condition.

Thread Rolling

Maximum tensile properties may be obtained by thread rolling after aging. However, usually it is preferred to thread roll as-drawn or annealed material, and then age harden. Material in the un-aged condition is more easily threaded, and subsequent aging tends to stress relieve the coldworked threads.

Reaming

Operating speeds for reamers should be about two-thirds of the speeds used for drilling. The reamer feed into the work should be 0.0015-0.004 in (0.04-0.1 mm) per flute per revolution. Feed rates too low will result in glazing and excessive wear. Conventional fluted reamers, flat solid reamers and insert tools for built-up reamers are made of high-speed steel. Composite tools with steel shanks tipped with cemented carbide are recommended.

Warping

Stresses produced during the machining process may result in distortion or warping. This can be minimized by reducing the machining speed and/or the depth of cut.

		High Speed Steel		Carbide						
Depth of Cut	and and a start and the start of the start o	Surface	ri dri dri dri d attain attain attain	and a stand of the stand of the stand	Surface					
St. St. St. St. St. St.	Tool Material	Speed	Feed	Tool Material	Brazed Tool	Throw-Away	Feed			
in (mm)	Material	f t/min (m/min)	in/rev (mm/rev)	Material	ft/min (m/min)	ft/min (m/min)	in/rev (mm/rev)			
0.25 (6.4)	T-5	12-18 (3.7-5.5)	0.010 (0.25)	C-2	30-40 (9.1-12.2)	40-60 (12.2-18.3)	0.010 (0.25)			
0.05 (1.3)	M-36	15-20 (4.6-6.1)	0.008 (0.20)	C-2	40-50 (12.2-15.2)	50-100 (15.2-30.5)	0.008 (0.20)			

Table 17-Machining Parameters for INCONEL alloy 725*

*Annealed or aged material. Hardness range, approximately 85 Rb to 40 Rc. Water base, oil emulsion or chemical solution as cutting fluid.

Available Products and Specifications

INCONEL alloy 725 is designated as UNS N07725. The product is available as round bar and wire.

Bar and wire - ASTM B 805, ASME Code Case 2217

Bar and forging stock - SMC specification HA91, ASME Code Case 221/

Publication No. SMC-066 Copyright © Special Metals Corporation, 2005 (Dec 05)

INCONEL, INCOLOY, INCO-WELD, and 725NDUR are trademarks of the Special Metals Corporation group of companies.

The data contained in this publication is for informational purposes only and may be revised at any time without prior notice. The data is believed to be accurate and reliable, but Special Metals makes no representation or warranty of any kind (express or implied) and assumes no liability with respect to the accuracy or completeness of the information contained herein. Although the data is believed to be representative of the product, the actual characteristics or performance of the product may vary from what is shown in this publication. Nothing contained in this publication should be construed as guaranteeing the product for a particular use or application.